Effect of implant number and distribution on load transfer in implant-supported partial fixed dental prostheses for the anterior maxilla: A photoelastic stress analysis study

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The anterior edentulous maxilla may be treated with traditional methods such as a Kennedy Class IV removable dental prosthesis or a partial fixed dental prosthesis (PFDP).1 Prosthodontic rehabilitations of 6 consecutively missing anterior teeth are often associated with preparation-induced trauma or reduced patient satisfaction.2

Implant-supported PFDPs represent an alternative treatment option.2–4 Even though successful results have been reported for the rehabilitation of anterior teeth using single-tooth implants, opinion varies regarding the design of implant-supported PFDPs in the anterior maxilla.1–5

Renouard and Rangert1 suggested 4 different prosthesis designs when 4 maxillary anterior teeth are missing, with the smile line, vertical bone loss, gingival biotype, and mucosal thickness as risk factors. Their treatment options are 4 single implants, 4 splinted implants, a 4-unit PFDP supported by 2 implants in the lateral incisor positions, and a 4-unit cantilever PFDP with 2 implants in the central incisor positions. Krennmair et al2 investigated the clinical results and patient satisfaction with a 2-implant-supported 4-unit anterior PFDP consisting of central ovate pontics and lateral incisor implants. They found high implant survival and success rates and acceptable soft tissue health and periimplant conditions. Corrêa et al4

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MATERIAL AND METHODS

A photoelastic model of the human maxilla with an anterior edentulous region was made with photoelastic resin (PL-2; Vishay Micro-Measurements) by using a master mold and the pour acrylic resin technique.18–20

The life-size model included the hard palate and alveolar ridges. The first premolars were placed at the boundary of the edentulous region in the root sockets, and the posterior molars were omitted for convenience for both model fabrication and stress observation.

Six straight implants (OsseoSpeed 4.0 mm platform 11 mm length; Astra Tech AB) were placed in the 6 anterior tooth positions. The positions of the implants were determined by using a diagnostic waxing and surveying the duplicated stone cast. The central and lateral incisors were symmetrically placed at a 60-degree angle to the base of the maxilla around the midline, 3 mm from the adjacent implants and 2 mm lingually to the labial bone. The canines were placed at a 60-degree angle to the base of the maxilla and 2 mm mesial to the first premolars. The interpremolar width in this model was 40 mm, and the anteroposterior spread among the 6 implants was 10 mm. The platform surfaces of the implants were located 1 mm above the alveolar bone.

Impression copings (Implant Pick-up 3.5/4.0; Astra Tech AB) were connected to the implants, and a master mold was fabricated with a replication silicone (KE1300; Shin-Etsu). Then, impression copings in the silicone mold were connected with 6 implants. Photoelastic resin (PLM-1; Vishay Micro-Measurements) with an elastic modulus similar to tooth structure. The premolars were bonded to the sockets of the maxillary photoelastic model after a week of polymerization (Fig. 1).

Six individual abutments were fabricated using gold copings (cast-to abutments; Astra Tech AB), cast with type III gold alloy (V-Delta SF; Cendres Métaux SA), and customized with a milling machine (PF-200; Cendres Métaux SA). The superstructure for a cement-retained 6-unit PFDP was fabricated with dental Au-based metal ceramic alloys (V-Gnathos Plus; Cendres Métaux SA) (Figs. 2, 3).

In a photoelastic model with 6 implants, 5 different experimental models were developed with one 6-unit implant-supported PFDP at a time by connecting abutments to the specific implants. The experimental models with different number and position of the implants were summarized in Table 1.

Abutments were connected in the selected implant positions with a 20 Ncm torque, and the 6-unit PFDP was delivered with interim cement (Cavitex; Kerr Corp). A load of 127.4 N was applied at 3 loading points on the PFDP with a 30-degree-angle to the long axis of the implants: lingual third of left canine (P1), left lateral incisor (P2), and left central incisor (P3). The loading

Clinical Implications

Reduced stresses are associated with the 4-implant-supported partial fixed dental prosthesis (PFDP) design than the 2- or 3-implant-supported PFDP, whereas little difference was found between models 2C2CI (2 canines and 2 central incisors) and 2C2LI (2 canines and 2 lateral incisors).
points were formed 1 mm deep with No. 6 round burs (Fig. 4).

Before the experiments, the photoelastic model was inspected in the field of a circular polariscope (Vishay Micro-Measurements) to ensure that the model was stress free. To minimize surface refraction, the photoelastic model was positioned with a jig in a transparent plastic tank filled with mineral oil, and a load of 127.4 N was applied on the loading point with a static loading device (Seiki) (Fig. 5). Stresses that developed in the supporting structure were monitored photoelastically in the field of the circular polariscope and recorded photographically with a digital camera (D100; Nikon Inc). After each loading, there was a 5-minute resting period to allow the residual stress to disappear, and trials were conducted more than 2 times to ensure reproducibility. Recording was conducted on the front, right, and left sides.

Using the digital images of the 5 models, fringe orders (FOs) were estimated and compared in the distocervical part, apical part, and mesiocervical part of the implants (Fig. 6). The FO was measured at 18 measuring points in total with reference to the isochromatic fringe characteristics shown in Table 2.

**RESULTS**

In a maxilla with an anterior edentulous region, 6 implants were placed and restored with a 6-unit PFDP according to 5 different design concepts. The FOs around the implant supporting tissue were observed using photoelastic stress analysis, and the results are shown in Figure 7.
The 6-implant-supported PFDP (model 6I) showed the most even distribution and lowest stresses in all the loading conditions. With a decrease in implant number, the stresses around the implants increased.

When the canine was loaded (P1), the 2- or 3-implant-supported PFDPs (model 2C and 2C1CI) exhibited higher stresses of 3 FO around the implants at the canine position than did the 4- or 6-implant-supported PFDPs (model 6I, 2C2CI, and 2C2LI). Apical stresses of 2.5 FO (model 6I) or 2.65 FO (model 2C2CI and 2C2LI) were observed around the implants at the canine position.

When the lateral incisor was loaded (P2), the apical stresses around the implants at the canine position of each model decreased in the following order: 2.0 FO (model 2C), 1.82 FO (model 2C2CI and 2C1CI), 1.22 FO (model 6I and 2C2LI). However, the implant at the lateral incisor position showed higher stresses with model 2C2LI (1.39 FO) than model 6I (1.22 FO). In addition, the implant at the central incisor position showed higher stresses with model 2C1CI (1.22 FO) than model 2C2CI (1.0 FO).

When the central incisor was loaded (P3), the apical stresses around the implants at the canine position in 4 models were below 1.0 FO, except in the case of model 2C (1.82 FO). The apical stresses around the implants at the central incisor position increased in model 2C1CI (1.82 FO) and model 2C2CI (1.39 FO). The apical stress around the implants at the lateral incisor position of model 2C2CI was 1.22 FO.

DISCUSSION

The null hypothesis of this study was rejected based on the biomechanical differences among the implant-supported PFDPs with different numbers and locations in the anterior maxilla. The anterior maxilla is more critical for implant loss than other sites, and the failure rate of implants is often related to type III bone quality with thin cortical plate and dense trabecular bone in the premaxilla.1,9,10 The yield strength for cortical bone is 104 to 169 MPa, whereas that of trabecular bone is 82 to 133 MPa.11 The combination of poor bone quality and
overload was considered to be the leading cause of late implant failure.

The 6-implant-supported PFDP (model 6I) showed the most even distribution and lowest stresses in all loading conditions in this study. However, Avrampou et al\textsuperscript{17} reported that only 23\% of patients fulfilled bone volume classification for fixed type implant prostheses in the edentulous anterior maxilla. Therefore, the mesiodistal distance in the anterior maxilla is not sufficient to allow for the placement of 6 implants, 1 for each lost tooth, and implant-supported PFDPs are associated with pontics to optimize spacing and improve esthetics and reduce cost.\textsuperscript{2,4,7}

In biomechanical terms, limited information is available on the optimum number and location of implants on a fixed prosthesis for the anterior maxilla. Using 3D FEM, Corrêa et al\textsuperscript{4} compared 3 different implant locations in the maxilla. They reported that the group with 2 implants in the lateral incisor positions and anterior pontics (IL group) limited the displacement of the bone structure compared with other configurations under 45-degree loads of 150 N. The peak strain of 10 με was exhibited at the mesiolabial crest of the lateral incisor implants in the IL group, whereas the peak strain of 13 με was observed extensively at the labial and mesial crest around the group with central incisor implants with distal cantilevers (IC group). However, the cortical and trabecular bone were not overloaded in any of the groups, because these values were below the limit considered an overload.\textsuperscript{12} They emphasized that the appropriate positioning of dental implants can help avoid cantilever and mechanical overload and prevent failures.

Bidez and Misch\textsuperscript{5} demonstrated that the arch form of the maxilla influenced the treatment plan of the edentulous premaxilla. Three typical dental arch forms for the maxilla are square, ovoid, and tapering. As the lateral and central incisors were not cantilevered facially, 2 implants in the canine position might be sufficient for a square arch. In an ovoid arch, 3 implants should be in the premaxilla with 2 implants in the canine positions and at least 1 additional implant, preferably in a central incisor position. The anterior teeth were cantilevered far facially from the canine position in a tapering arch, with increased forces during mandibular excursions. As such, 4 implants in the bilateral canine and central incisor position should be considered to replace the 6 anterior teeth. In this study, the anteroposterior spread of the 6 implants was 10 mm, which is classified as an ovoid type arch form.

For an implant-restoration complex replacing 6 anterior teeth, the most important abutments might be the terminal canine abutments. If an implant-supported PFDP is loaded, the closest implant to the loading point would generally bear most of the load.\textsuperscript{9,19} When the canine was loaded, the 2- or 3-implant-supported PFDPs (model 2C and 2C1CI) showed higher stresses of 3 FO around the implants at the canine position than the 4- or 6-implant-supported PFDPs (model 6I, 2C2CI, and 2C2LI). When the central incisor was loaded, 2- or 3-implant-supported PFDPs (model 2C and 2C1CI) showed 1.82 FO around the implants at the canine or central incisor position, whereas the 4-implant-supported PFDPs (model 2C2CI and 2C2LI) showed similar levels of stresses with 1.22 to 1.39 FO around the implants at the incisor position. Although the stress on the canine decreased in model 2C1CI compared with model 2C at p2 and p3 conditions, 4-implant-supported PFDPs are safe with stresses less than 1.5 FO. Cantilevers in the facial and/or mesial direction can be a force magnifier and represent an important risk factor for complications in implant dentistry, including frequent screw loosening, prosthetic fracture, and crestal bone loss.\textsuperscript{6} Therefore, in most instances, the completely edentulous anterior maxilla should be restored with 4 implants splinted together to replace the anterior 6 teeth and to sustain the forces created during mandibular excursions.

The intermediary abutments are also important to limit the edentulous spans to the equivalent of less than 3 pontics. Three adjacent pontics are contraindicated because 3 pontics will flex 19 times more than 2-pontic restorations.\textsuperscript{2} In comparison with two 4-implant-supported PFDPs (model 2C2CI and 2C2LI), under p1 conditions, the stresses around canine position implants were similar. Under p2 conditions, model 2C2CI showed higher stresses of 1.82 FO around the implant at the

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canine position than seen in model 2C2LI. Under p3 conditions, model 2C2CI showed stresses of 1.39 FO around the implant at the central incisor position, whereas model 2C2LI showed stresses of 1.22 FO around the implant at the lateral incisor position. As a result, model 2C2CI and 2C2LI showed similar stress magnitudes around the implants at the incisor positions. However, in most instances, placing 2 neighboring

implants at the central incisor positions critically influences the esthetics of the PFDPs and the face overall. Inappropriate positioning results in midline shift, causing further difficulties with esthetics. As the intermediary abutment, the lateral incisor position should be considered preferable to the central incisor positions.

The results presented in this study are consistent with those in the study by Bölükbaşı and Yeniyol. Using a 3D FEM, they investigated the effect of dental implant localizations in the anterior maxilla on the strain values around implants. They compared 5 different PFDP designs for maximum strain values at the cortical bone under 45-degree loads of 100 N. The highest strain values were measured as follows: 3037 microstrain in the model with 2 canines; 1973 microstrain for model with 2 canines and a central incisor; 1596 microstrain for model with 2 canines and 2 central incisors; 1644 microstrain for model with 2 canines and 2 lateral incisors. They concluded the model with 2 canines and 2 lateral incisors was the least risky method in biomechanical terms because the microstrain value around the lateral incisor was lower than that around the central incisor.

Little has been reported on implant-prosthodontic rehabilitation in patients with 6 missing anterior teeth, with only some suggestions on the number and position of anterior implants as a part of the treatment of the fully edentulous maxilla. Sagat et al used 3D FEM to determine the most advantageous implant localizations in fixed implant-supported prostheses supported by 6 or 8 implants in the edentulous maxilla with 5 different alveolar arch forms. The most favorable implant distribution for anterior loading was the 8 implant group with lateral incisor, canine and 2 premolars in 4 alveolar arch models.

Various studies have evaluated the bone quality of the premaxilla. Fuh et al determined the trabecular bone density at potential implant sites in different regions of the Chinese jawbone using computed tomography images and reported that the bone densities in the anterior maxilla were approximately equal to those in the anterior mandible. The bone densities in the 2 regions were 530 ±161 HU for the anterior mandible and 516 ±132 HU for the anterior maxilla. Wakimoto et al investigated the characteristics of implant sites on the edentulous alveolar ridge in the anterior maxilla. They studied the bone...
quantity and quality of implant sites at the anterior maxilla using CT images of the implant sites on 33 patients who underwent dental implant therapy. No maxillary sites were judged to have a bone quality of 1 in their group. Quality 3 accounted for 69.7% of the total samples. Canines displayed greater alveolar bone widths than did the incisors, whereas incisors had higher bone densities than canines.

The occlusal force during mastication and swallowing in natural dentition and implants varies. Haroldson et al. reported it to be 150 to 235 N and Paphangkorakit and Osborn reported 90 to 307 N. Waltimo and Könönen reported approximately 300 N as the maximum physiologic occlusal force, and in this study, a 127.4 N load was used. While the occlusal force may depend on the condition of the mandibular anterior region, this force is within the range of the average occlusal force of implants or natural dentition.

One of the limitations of this study is that the photoelastic models were not fabricated separately using the 5 different designs, but the same photoelastic model with 6 implants was used with different implant-supported PFDP designs. As a result, the stress on each implant is shown within a limited narrow region, and this situation may be different from clinical conditions. However, if different photoelastic models are fabricated, there may be differences among models. Therefore, the influence of different prosthetic design was evaluated within the same model to allow consistency. The advantage of photoelastic analysis is that it uses the actual prostheses and may be more accurate in simulating the clinical conditions.

However, representing the nonhomogeneous and anisotropic structure of bone with photoelastic models limits the predictions of the biological response to applied loads. This study showed that the amount and distribution of stress depended on the design of the prostheses. If the bone quality of the anterior maxilla is weak, there is a high degree of bone resorption and high occlusal forces such as bruxism. In these patients, additional implant placement should be considered in the anterior region when implant-supported PFDPs are designed.

CONCLUSIONS

This study used 3D photoelastic stress analysis to compare the biomechanical behavior of 5 different implant-supported PFDP designs. One photoelastic model with 6 implants placed in the anterior edentulous maxilla was used to maintain uniformity. Within the limitations of this study, implant number and distribution influenced stress distribution around implants in the anterior maxilla. The 6-implant-supported PFDP (model 6I) showed the most even and lowest stress distribution in all loading conditions. With a decrease in implant number, the stresses around implants increased. The 4-implant-supported PFDP design would be better than 2- or 3-implant-supported PFDPs, whereas little difference was found between models 2C2CI and 2C2LI.

REFERENCES


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